



Numerical Analysis on bullet Penetration Resistance of Heat Treated Lightweight C-grade Bulletproof Steel Plates

Zhang Jingwen
2014.08.22



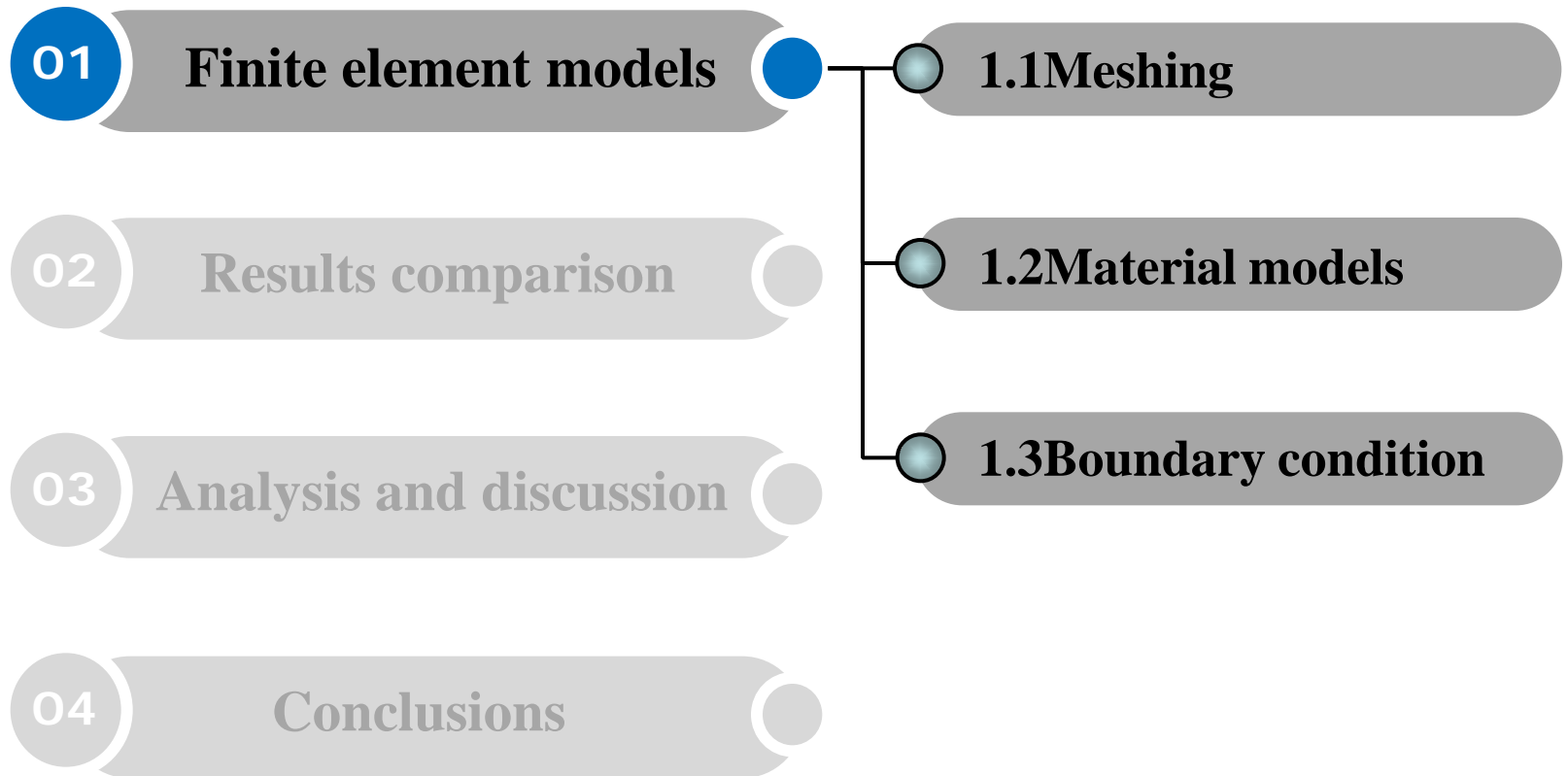


Contents

- 1** **Finite element models**
- 2** **Results comparison**
- 3** **Analysis and discussion**
- 4** **Conclusions**



1. Finite element models





1.1 Meshing

Outer diameter D of bullet : 7.62mm.

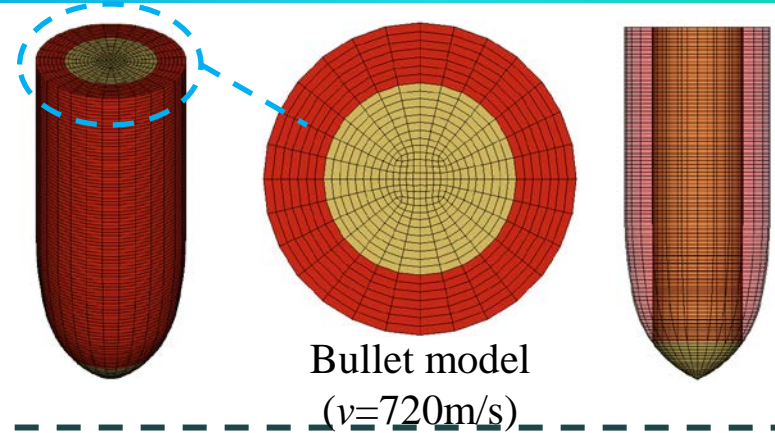
Outer diameter d of bullet core : 4.7mm.

Maximum element size: 0.8mm.

Minimum element size: 0.2mm.

Weight of bullet: 5.5g.

Bullet core and the outer layer are connected with the same nodes.



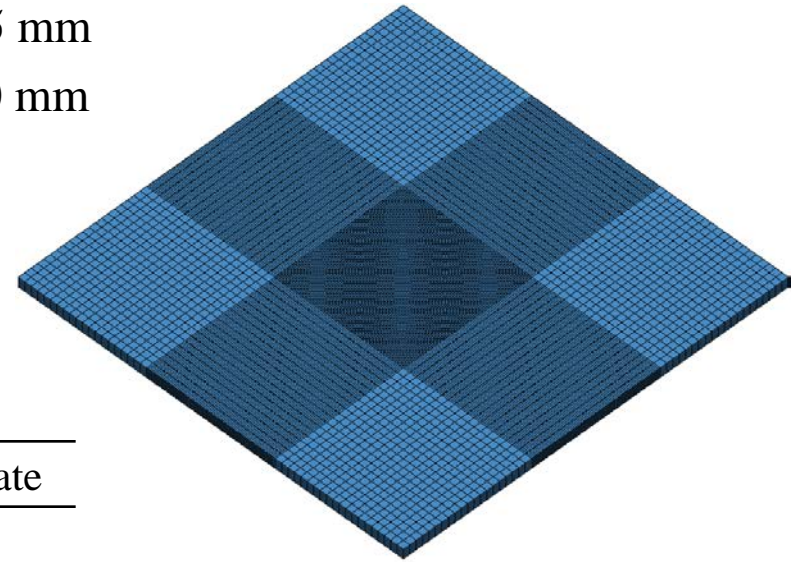
Actual size of the bulletproof steel plate :305mm × 305 mm

Model size of the bulletproof steel plate :120mm × 120 mm

Maximum element size: 2.0mm.

Minimum element size : 0.5mm.

Layer number of thickness direction: 4-8(according to different thickness)



Bulletproof Steel Plate model

Information	Bullet	Bulletproof Steel Plate
Node amount	44667	73205-131769
Element amount	43252	57600-115200



1.2 Material models

Bullet

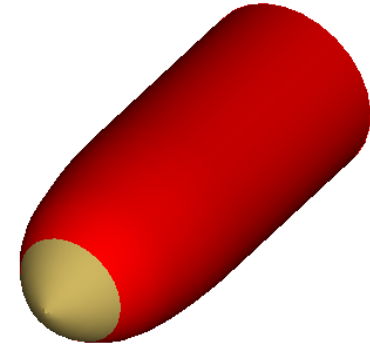
Bulletproof Steel Plate

Mat-Plastic-Kinematic

MATL3 in Dyna module of HyperMesh platform

Constitutive equation:
$$\sigma_Y = \left[1 + \left(\frac{\dot{\epsilon}}{c} \right)^{\frac{1}{P}} \right] (\sigma_0 + \beta E_P \epsilon_P^{eff})$$

$$E_P = \frac{E_{tan} E}{E - E_{tan}}$$



σ_Y —actual yield stress

σ_0 —initial yield stress

β —hardening parameter

C 、 P —strain rate parameter

ϵ_P^{eff} —effective plastic strain;

E —elastic modulus;

E_{tan} —shear modulus;

E_p —plastic hardening modulus.

Material parameters of bullet

Material parameter	Bullet outer layer	Bullet core
(kg/m ³)	7.8	7.8
γ	0.3	0.3
E (GPa)	210	210
σ_s (MPa)	235	345
Failure strain ϵ	1.2	1.2



1.2 Material models

Bullet

Bulletproof Steel Plate

Chemical composition of C-grade bulletproof steel plates

Steel	C	Si	Mn	P	S	Al	Nb+V+Ti	Cr +Ni	B
C-grade	0.38~0.44	0.31~0.37	1.15~1.25	≤0.015	≤0.015	0.046	≥0.114	≥1.0	0.0016

Hot stamping technology was listed in Ref.[7].

Material parameters of bulletproof Steel Plate

MAT-simplified-Johnson-Cook
 MATL98 in Dyna module of HyperMesh platform
 Effect of temperature is not considered.
 Constitutive equation:

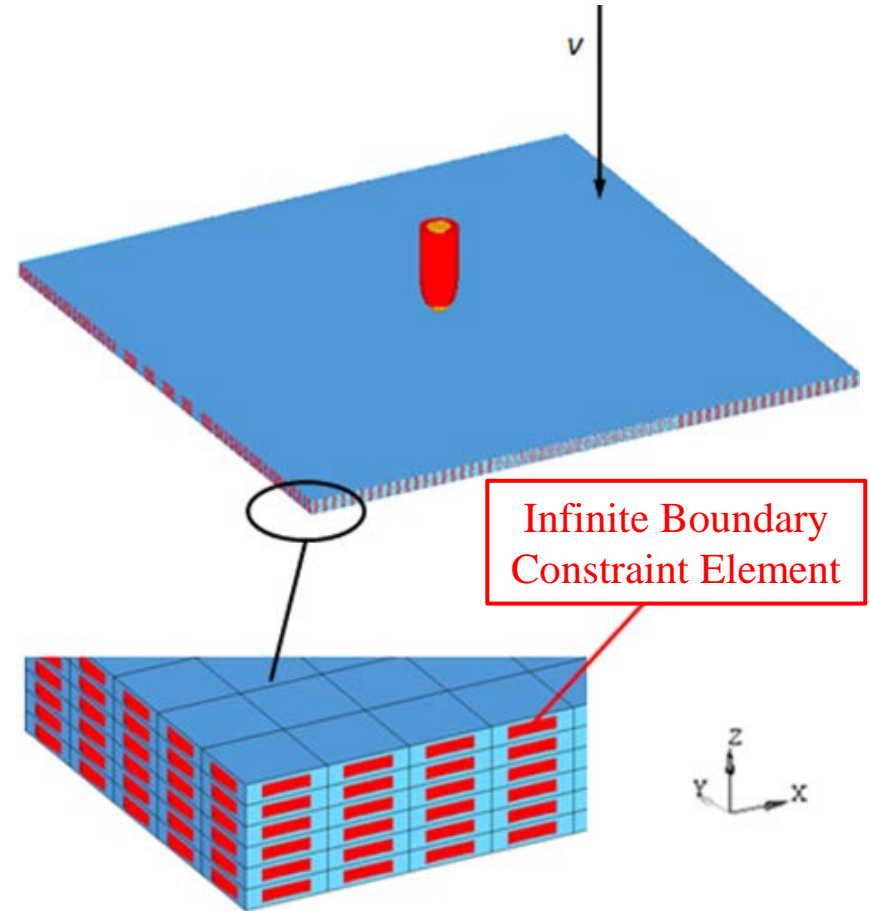
$$\sigma = (A + B\varepsilon^n) \left(1 + C \ln \frac{\dot{\varepsilon}}{\dot{\varepsilon}_0}\right) (1 - T^{*m})$$
 σ —equivalent stress;
 ε —equivalent strain;
 A, B, C, n —material parameters;
 $\dot{\varepsilon}$ — effective plastic strain rate
 $\dot{\varepsilon}_0$ —referring strain rate

Material parameter	Material No.		
	C1	C2	R
(kg/m ³)	7.8	7.8	7.8
γ	0.3	0.3	0.3
E (GPa)	204	197	206
σ_s (MPa)	1515	1400	1470
Tensile stress (MPa)	2200	2035	1775
Fracture elongation	0.063	0.052	0.058
Johnson-Cook constitutive models of steel plates			
Material	Johnson-Cook constitutive models		
C1	$\sigma = (1670 + 3197\varepsilon^{0.0525}) \left(1 + 0.00414 \ln \frac{\dot{\varepsilon}}{\dot{\varepsilon}_0}\right)$		
C2	$\sigma = (1500 + 3536\varepsilon^{0.5477}) \left(1 + 0.0043 \ln \frac{\dot{\varepsilon}}{\dot{\varepsilon}_0}\right)$		
R	$\sigma = (1600 + 1328\varepsilon^{0.5238}) \left(1 + 0.005724 \ln \frac{\dot{\varepsilon}}{\dot{\varepsilon}_0}\right)$		



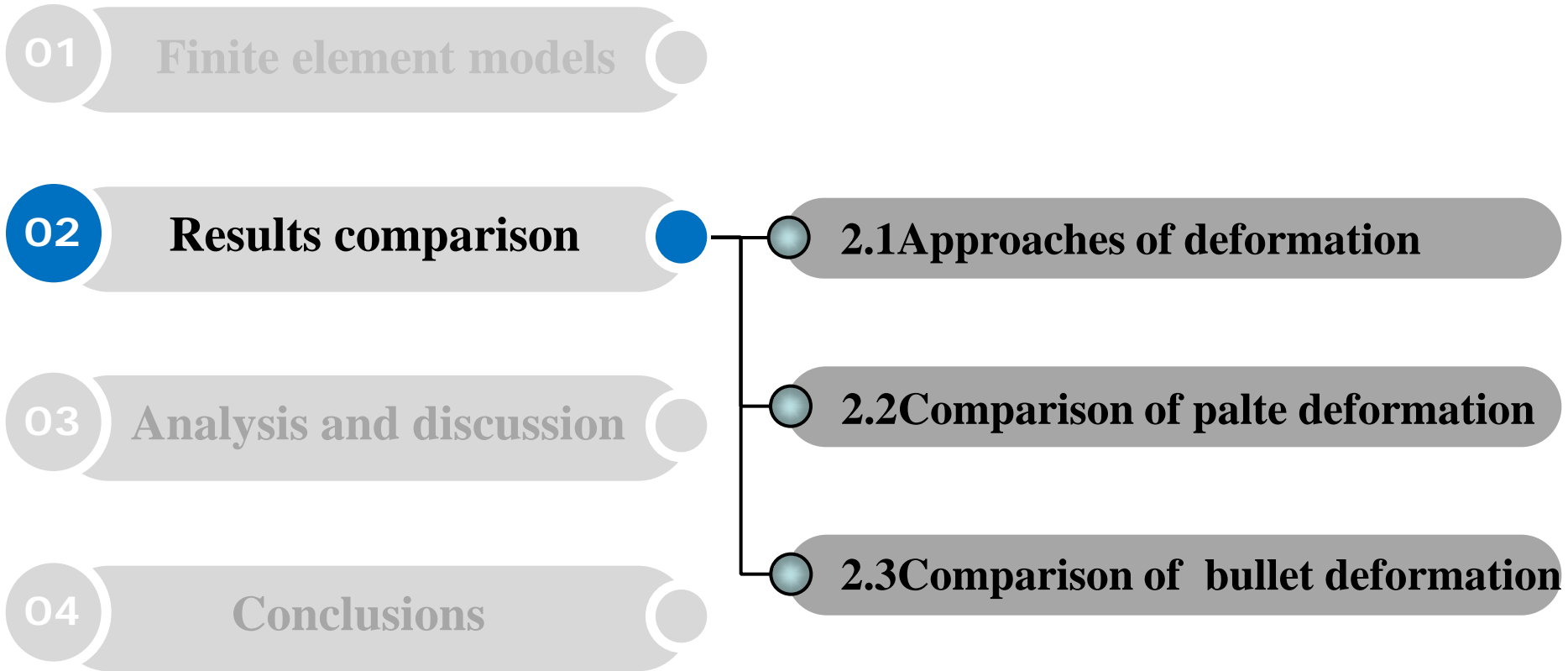
1.3 Boundary condition

- Bullet restriction: NO.
- Incident direction: Z
- Velocity: 720m/s
- Steel plate restriction: Infinite Boundary
- Constraint Element
- Contact : Face to face
- Total computing time : 100 μ s
- Time step: 2 μ s
- Output data: Velocity
Force
Energy





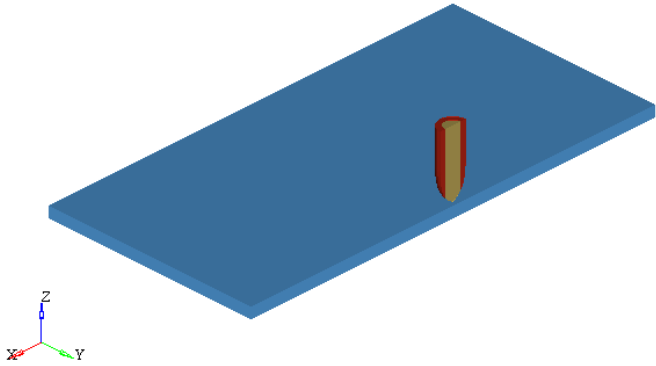
2. Results comparison





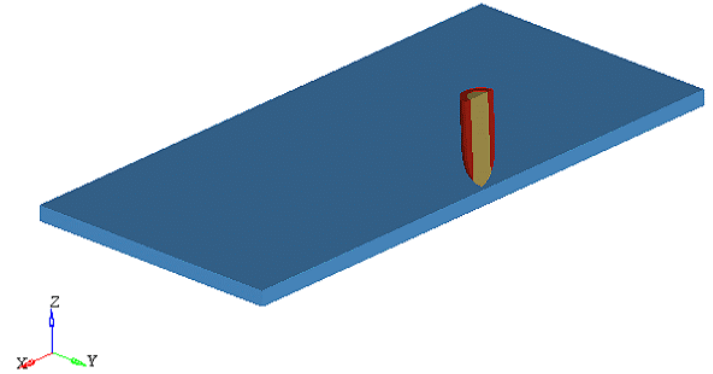
2.1 Approaches of deformation

LS-DYNA user input
Result : E:\bullet\mode\c2\c2_3.1_720\c1_3.1_720.h3d
Loadcase 1 : Time = 0.000000
Frame 1



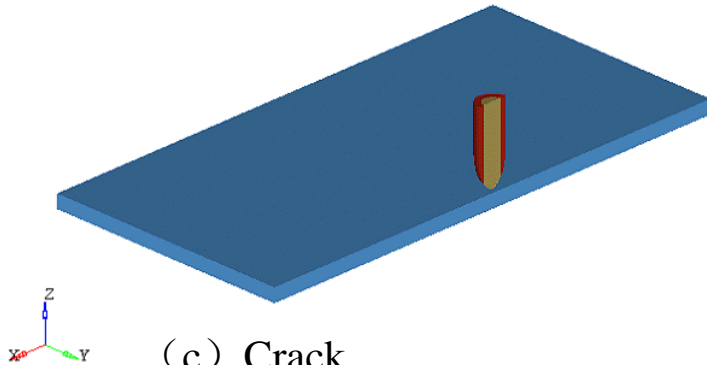
(a) Thoroughly penetration

LS-DYNA user input
Result : D:\zjw\case2\b2\b2_3.3_720\b2_3.3_720.h3d
Loadcase 1 : Time = 0.000000
Frame 1



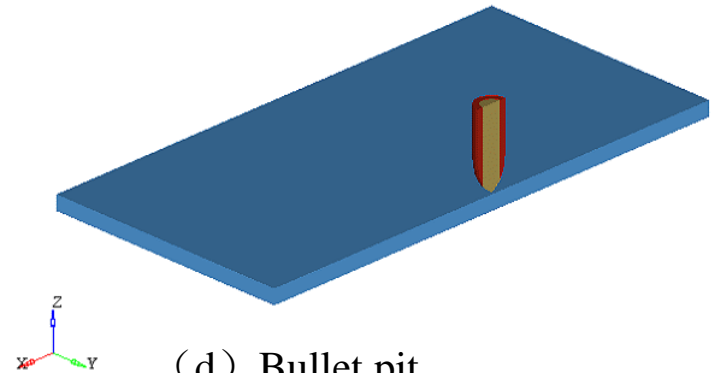
(b) Rear collapse

LS-DYNA user input
Result : D:\zjw\case2\c1\c1_3.3_720\c1_3.3_720.h3d
Loadcase 1 : Time = 0.000000
Frame 1



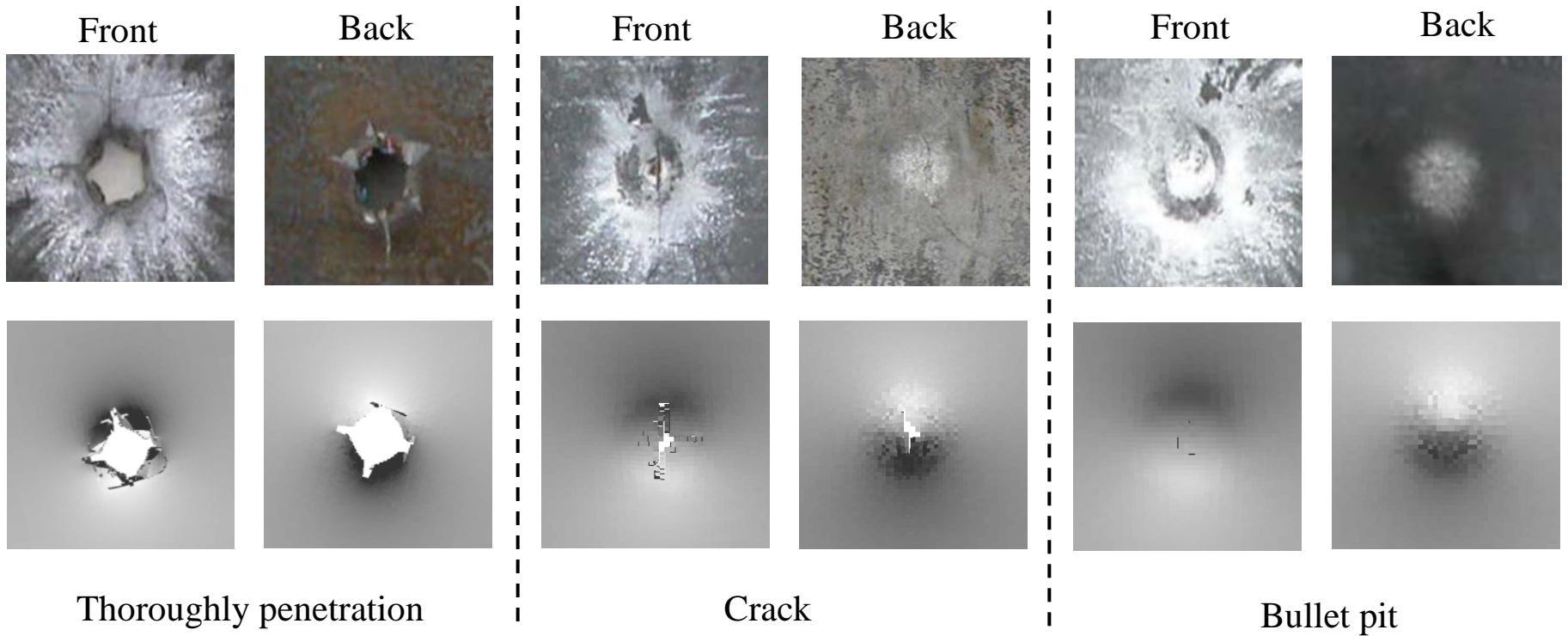
(c) Crack

LS-DYNA user input
Result : D:\zjw\case2\c1\c1_3.5_720\c1_3.5_720.h3d
Loadcase 1 : Time = 0.000000
Frame 1



(d) Bullet pit

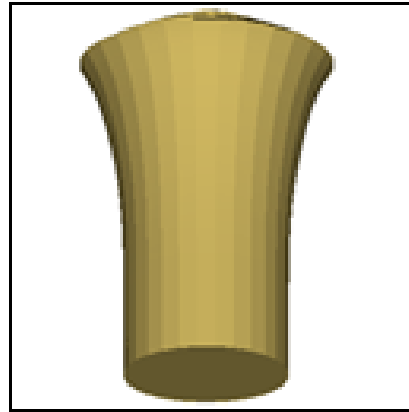
2.2 Comparison of plate deformation



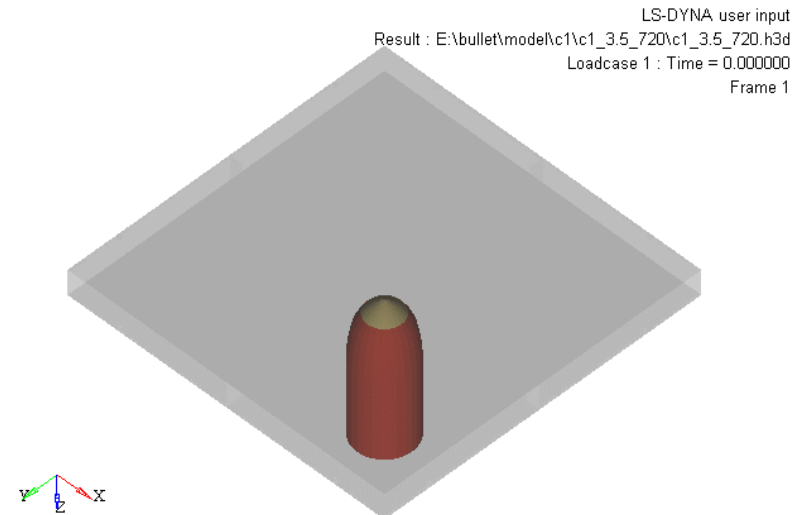
- ◆ The shape of bullet holes are very similar when thoroughly penetration occurs.
- ◆ The orientation of cracks are basically the same when cracking occurs.
- ◆ Even yielding bullet pits, there's no obviously difference.



2.3 Comparison of bullet deformation

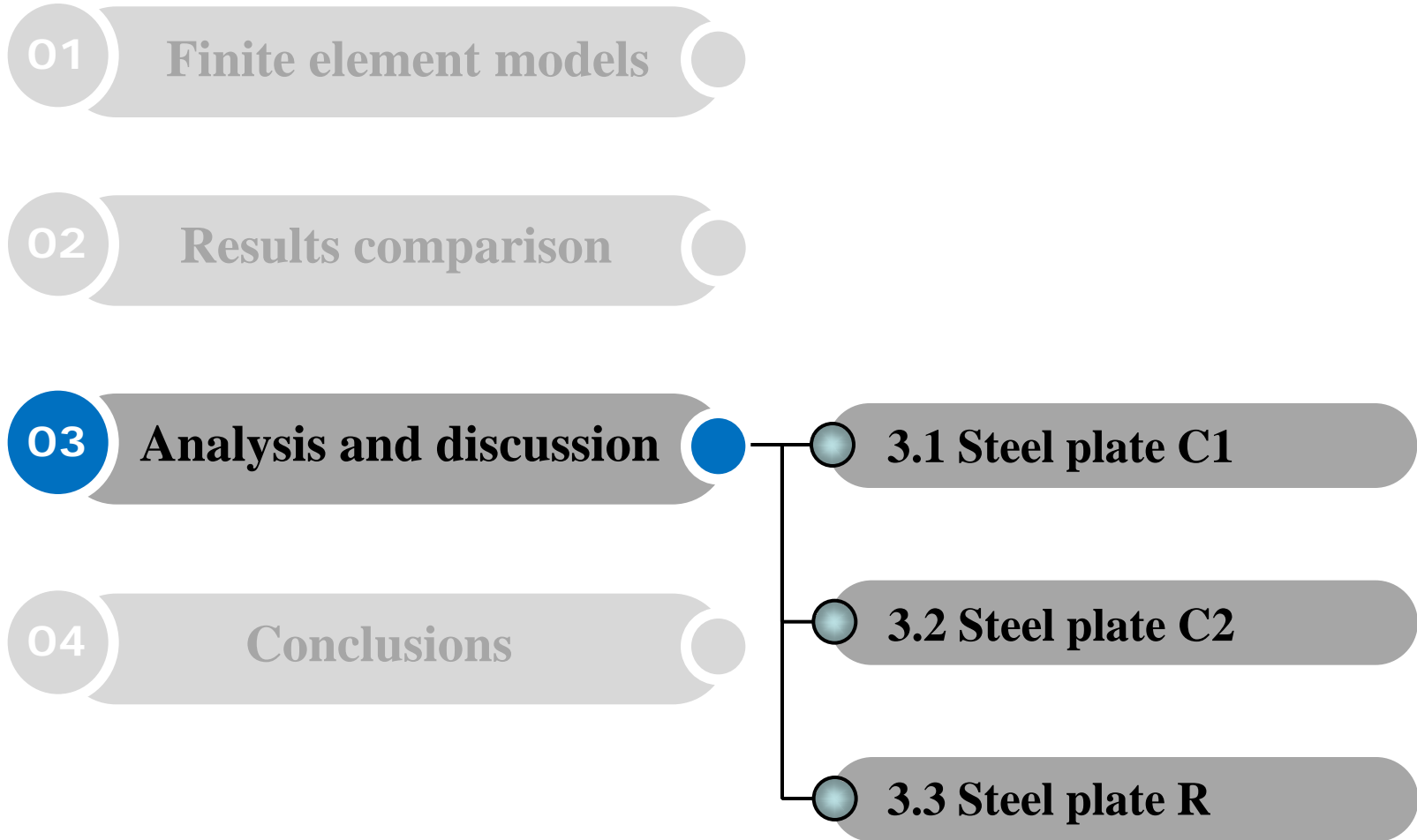


Comparison of bullet core between simulation and experiment at the speed of 720m/s





3. Analysis and discussion

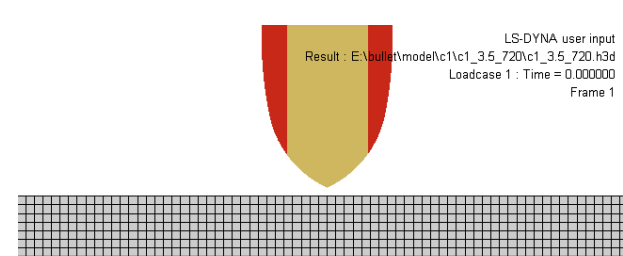
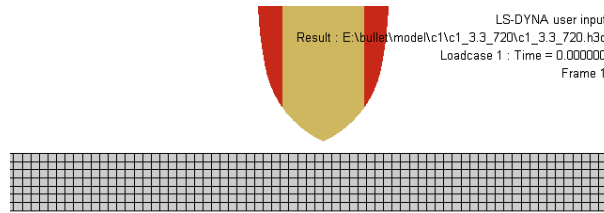
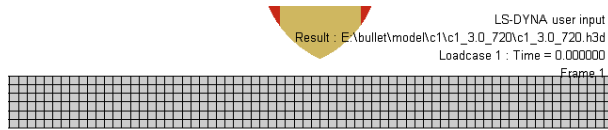




3.1 Steel plate C1

Simulation results of steel plate C1

Bullet speed (m/s)	Plate thickness t (mm)	Deformation mode	Deformation height h (mm)	Energy absorption of plate (J)	Maximum contact force (KN)	Residual speed (m/s)	Energy absorption of bullet (J)
720	3.0	Thoroughly penetration	11.0	486	150	86	240
	3.1-3.4	crack	7.2-10.3	516-530	161-164	0	245-268
	3.5	Yielding bullet pit	6.8	545	166	0	276



Thickness: 3.0mm



Thickness: 3.3mm



Thickness: 3.5mm



3.2 Steel plate C2

Simulation results of steel plate C2

Bullet speed (m/s)	Plate thickness t (mm)	Deformation mode	Deformation height h (mm)	Energy absorption of plate (J)	Maximum contact force (KN)	Residual speed (m/s)	Energy absorption of bullet (J)
	3.1	Thoroughly penetration	10.3	464	148	116	212
720	3.2-3.6	crack	7.3-10.2	522-527	153-160	0	236-272
	3.7	Yielding bullet pit	6.8	545	162	0	284



Thickness: 3.1mm

Thickness: 3.5mm

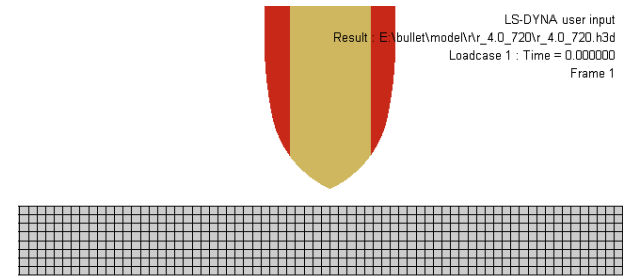
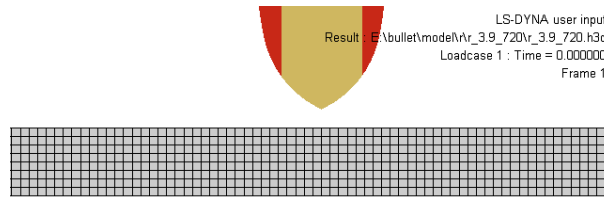
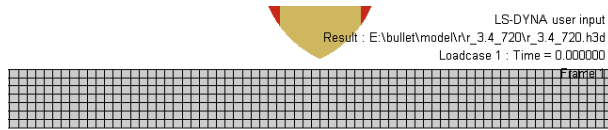
Thickness: 3.7mm



3.3 Steel plate R

Simulation results of steel plate R

Bullet speed (m/s)	Plate thickness t (mm)	Deformation mode	Deformation height h (mm)	Energy absorption of plate (J)	Maximum contact force (KN)	Residual speed (m/s)
720	3.4	Thoroughly penetration	9.7	410	153	47.2
	3.5-3.9	crack	6.8-8.6	464-476	155-167	0
	4.0	Yielding bullet pit	6.0	508	168	0



Thickness: 3.4mm

Thickness: 3.9mm

Thickness: 4.0mm



4. Conclusions

01 Finite element models

02 Results comparison

03 Analysis and discussion

04 Conclusions



4. Conclusions

- ◆ The constitutive equation considering the sensitivity of strain rate of material. Work hardening, strain rate hardening and dynamic yield stress equation with plastic hardening modulus are included in bullet material model and Johnson-Cook equation is applied to fit the stress-strain curves of bulletproof steel plates.
- ◆ The comparisons of bullet deformation, plate deformation and cracking all indicate the reliability of simulation results.
- ◆ When the plates C1, C2 and R with tensile strength of 2200MPa, 2035MPa and 1775MPa respectively are shoot at 720m/s, the limit thickness, simultaneously acquired by both simulation and experiment, are respectively 3.5mm, 3.7mm and 4.0mm.
- ◆ As a powerful method to analyze the limit thickness of bulletproof steel plate, numerical simulation effectively reduces work and cost.



Thanks!